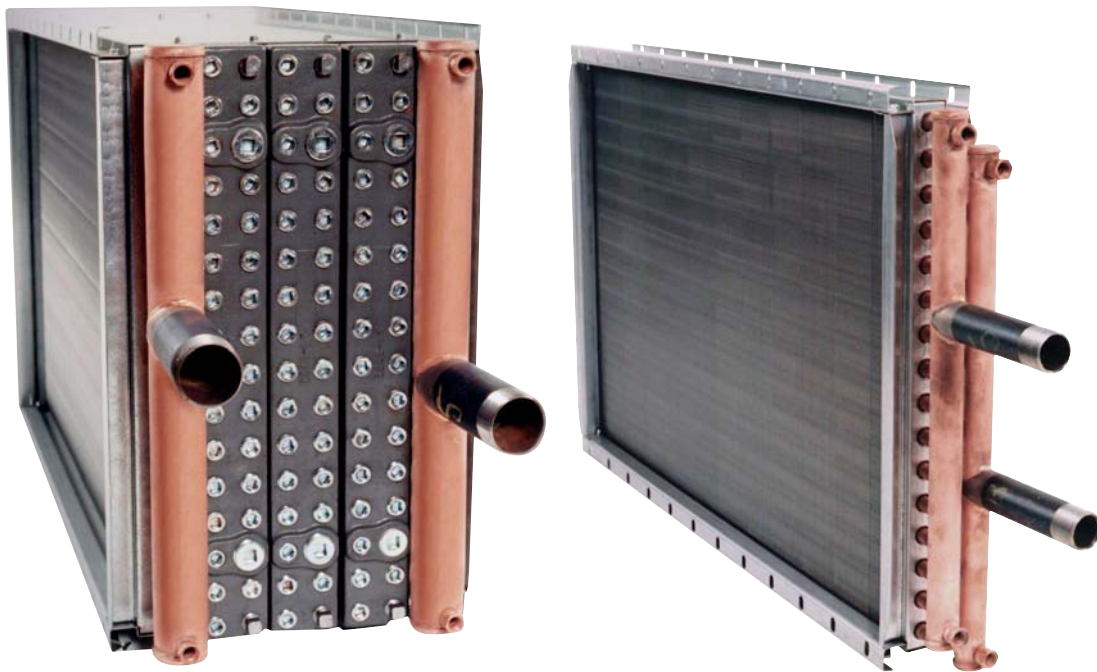




Trane Engineers Newsletter Live

Coil Selection and Optimization

Presenters: Brian Hafendorfer, Todd Michael, John Murphy, Jeanne Harshaw (host)





Trane Engineers Newsletter Live Series

Coil Selection and Optimization

Abstract

In this ENL program, Trane engineers will discuss the application, selection, and optimization of both chilled-water and hot-water coils. Topics include a discussion about the impact of both water and air velocities on coil performance, a review of example selections for chilled-water and hot-water coils to demonstrate the tradeoffs of cost, pressure drop, and capacity, and an overview of various methods to prevent water coils from freezing during cold weather.

Presenters: Trane engineers Brian Hafendorfer, Todd Michael, and John Murphy

After viewing attendees will be able to:

1. Identify the various configuration and construction options for chilled-water and hot-water coils
2. Understand the impact of both water and air velocities on coil performance
3. Evaluate water coil selection choices at various water temperatures and flow rates
4. Understand the balance of coil face area, airside pressure drop, and waterside pressure drop when selecting a coil
5. Properly protect water coils from freezing, when necessary

Agenda

- Water and air velocity ranges
- Coil selection examples
 - Chilled-water coils
 - Hot-water coils
- Freeze protection
- Summary



Presenter biographies

Coil Selection and Optimization

Todd Michael | heat transfer engineer | Trane

Todd Michael joined Trane in 1989 and is a Heat Transfer Engineer for air-to-refrigerant heat exchangers. His primary responsibility is to provide plate fin and round tube coil development expertise to project teams.

Todd received a Bachelor of Science Degree in Physics from Western Illinois University, and Bachelor Of Science and Master of Science Degrees in Mechanical Engineering from the University of Illinois at Urbana-Champaign. He is a member of ASHRAE and is the AHRI Forced-Circulation Air-Cooling and Air-Heating Coil Engineering Committee Chairman.

John Murphy | applications engineer | Trane

John has been with Trane since 1993. His primary responsibility as an applications engineer is to aid design engineers and Trane sales personnel in the proper design and application of HVAC systems. As a LEED Accredited Professional, he has helped our customers and local offices on a wide range of LEED projects. His main areas of expertise include energy efficiency, dehumidification, dedicated outdoor-air systems, air-to-air energy recovery, psychrometry, and ventilation.

John is the author of numerous Trane application manuals and Engineers Newsletters, and is a frequent presenter on Trane's Engineers Newsletter Live series. He has authored several articles for the ASHRAE Journal, and was twice awarded "Article of the Year" award. As an ASHRAE member he has served on the "Moisture Management in Buildings" and "Mechanical Dehumidifiers" technical committees. He was a contributing author of the Advanced Energy Design Guide for K-12 Schools and the Advanced Energy Design Guide for Small Hospitals and Health Care Facilities, a technical reviewer for the ASHRAE Guide for Buildings in Hot and Humid Climates, and a presenter on the 2012 ASHRAE "Dedicated Outdoor Air Systems" webcast.

Brian Hafendorfer | applications engineer | Trane

Brian joined Trane in 2000 and spent 8 years as a product engineer focused on coils for heating and cooling air with water, steam, and refrigerant for use in air handling systems. After joining the applications engineering team in 2008 his primary focus has been coils and air cleaning with a responsibility for developing and supporting integrated HVAC product solutions for Trane customers and providing a link between the sales, design, and manufacturing organizations.

Brian earned his Bachelor of Science in Mechanical Engineering from the University of Kentucky. As a licensed professional engineer he is an active member of ASHRAE and has served multiple committee positions for both "Ultraviolet Air and Surface Treatment" and "Gaseous Air Contaminants and Removal Equipment", and the project committee for ASHRAE Standard 62.1.



Coil Selection and Optimization

Trane Engineers Newsletter Live Series



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Learning Objectives

1. Identify the various configuration and construction options for chilled-water and hot-water coils
2. Understand the impact of both water and air velocities on coil performance
3. Evaluate water coil selection choices at various water temperatures and flow rates
4. Understand the balance of coil face area, air pressure drop, and water pressure drop when selecting a coil
5. Properly protect water coils from freezing, when necessary

Today's Presenters



John Murphy
Applications Engineer

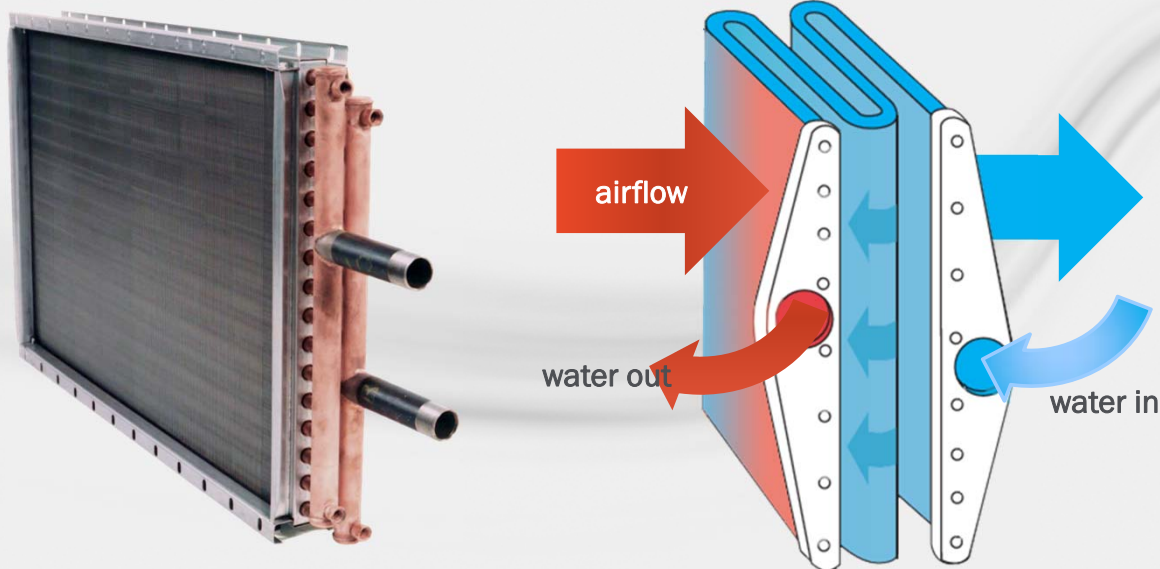


Brian Hafendorfer
Applications Engineer



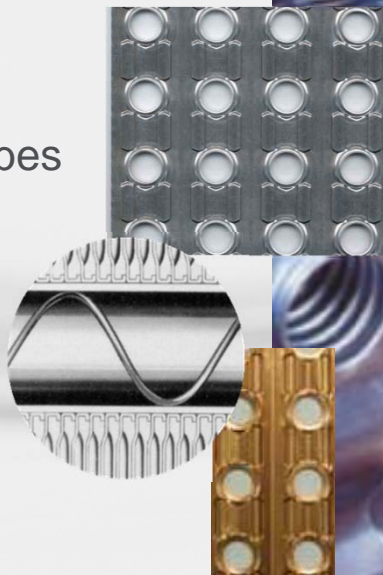
Todd Michael
Coil Heat Transfer
Engineer

Water Coils



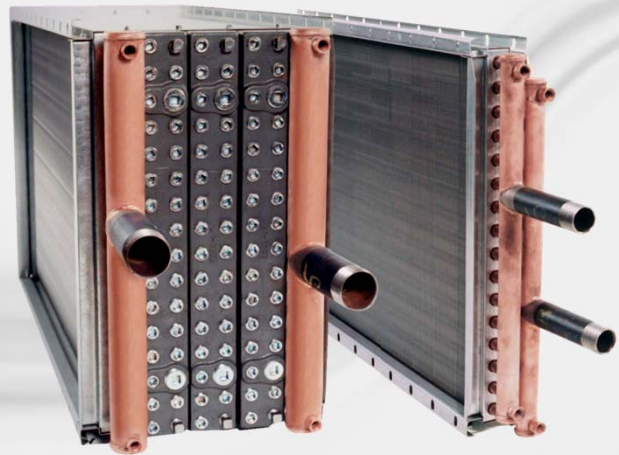
Configuration Options

- Coil face area
- Number of rows of tubes
- Tube diameter
- Number of fins
- Fin surface design
- Coil circuiting
- Turbulators



Construction Options

- Tube material
- Tube wall thickness
- Fin material
- Fin thickness
- Casing material
- Header type and material
- Coil coatings

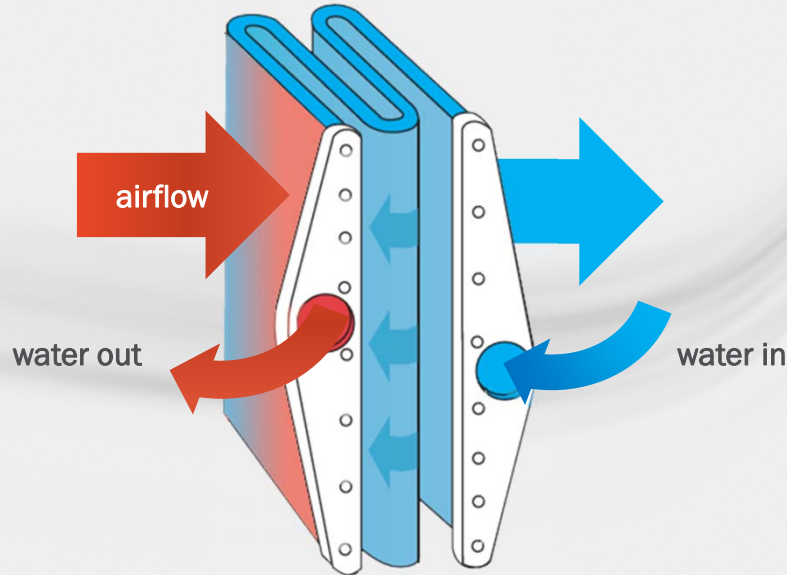


Agenda

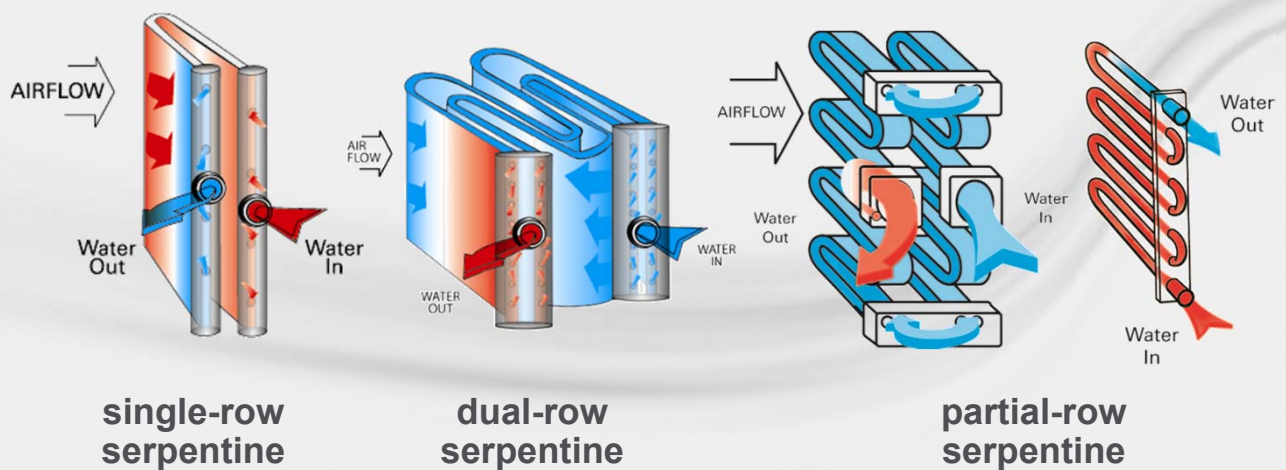
- Water and air velocity ranges
- Coil selection examples
 - Chilled-water coils
 - Hot-water coils
- Freeze protection



Water Flow Through Coils



Coil Circuiting



Water Velocity-Related Concerns

Water velocity too low:

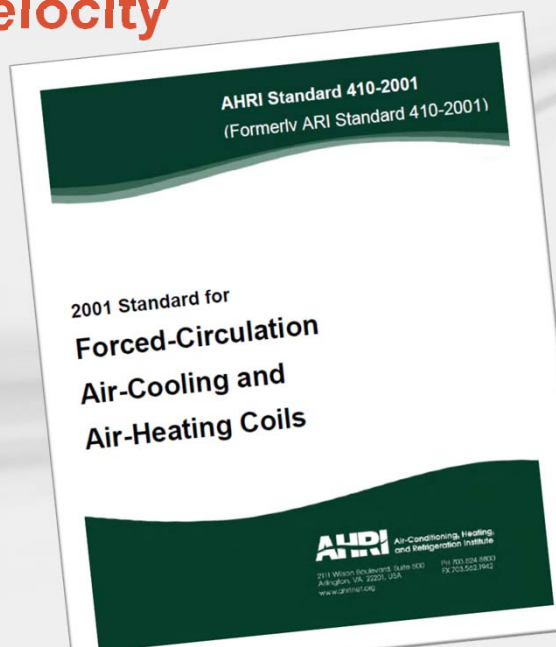
- Tube fouling
- Air trapped in the coil
- Poor water distribution
- Risk of freezing

Water velocity too high:

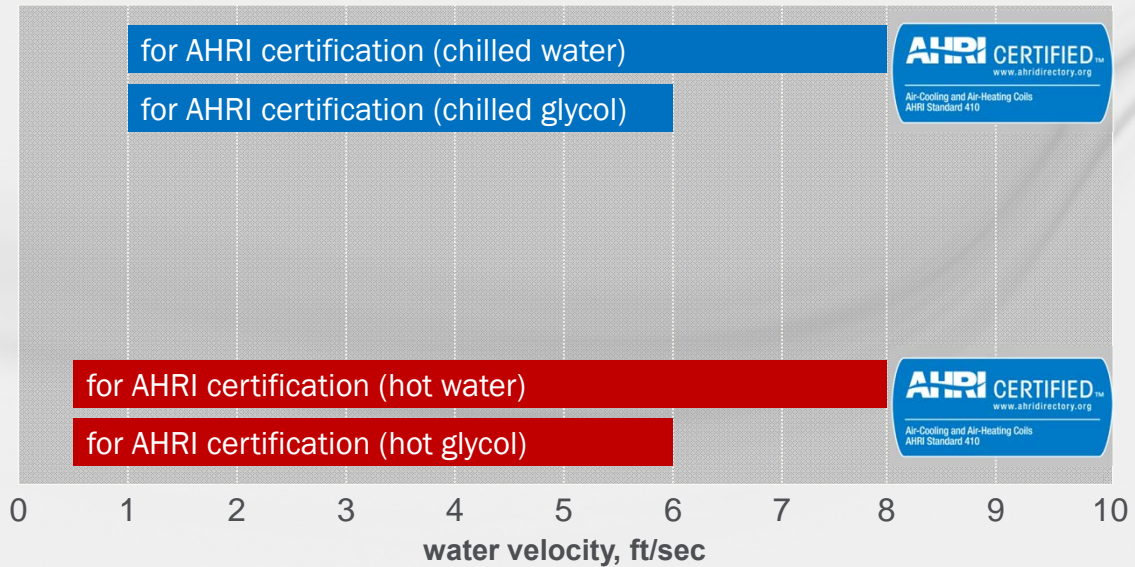
- Tube erosion
- High water pressure drop
- Noise

Guidelines for Water Velocity

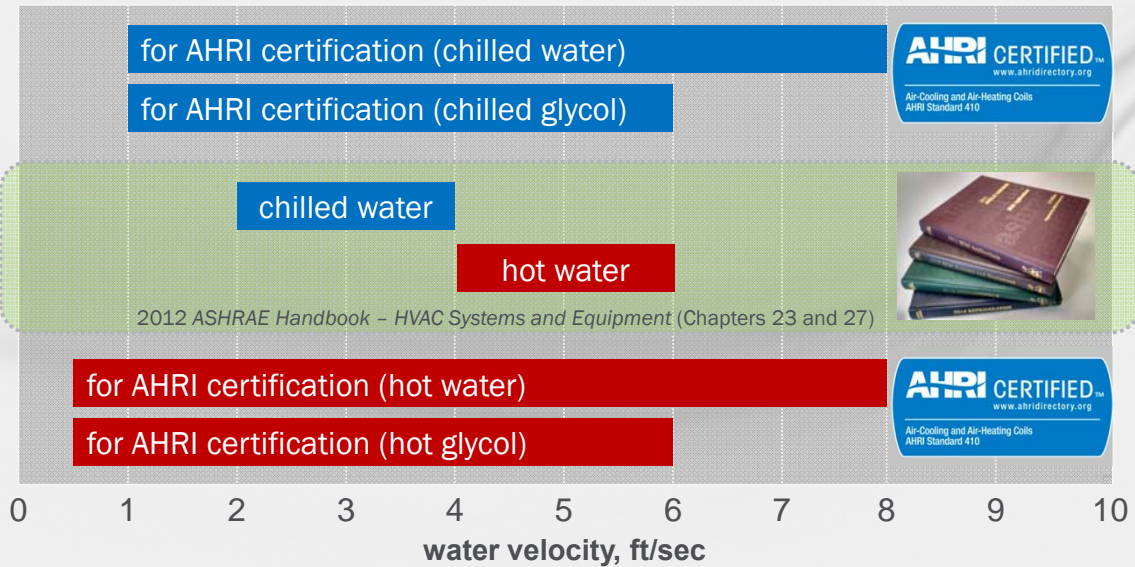
AHRI Standard 410
*Forced-Circulation Air-Cooling
and Air-Heating Coils*

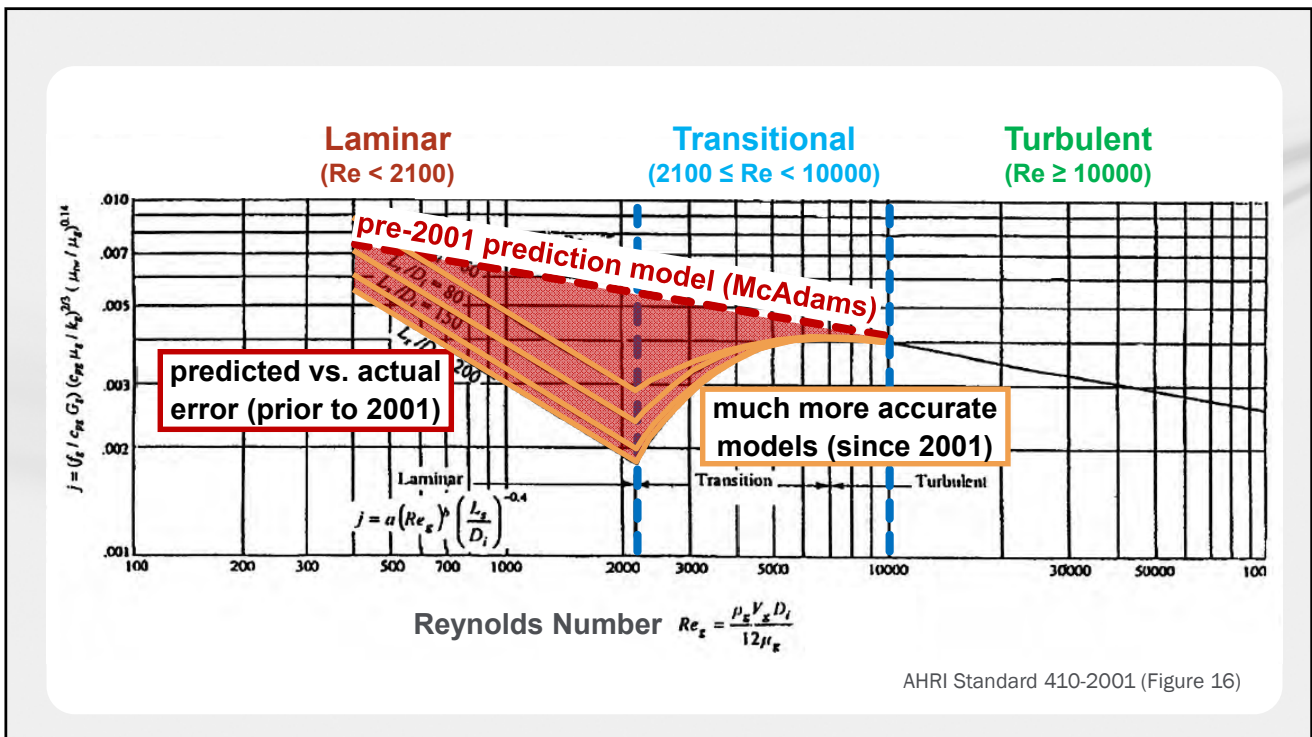
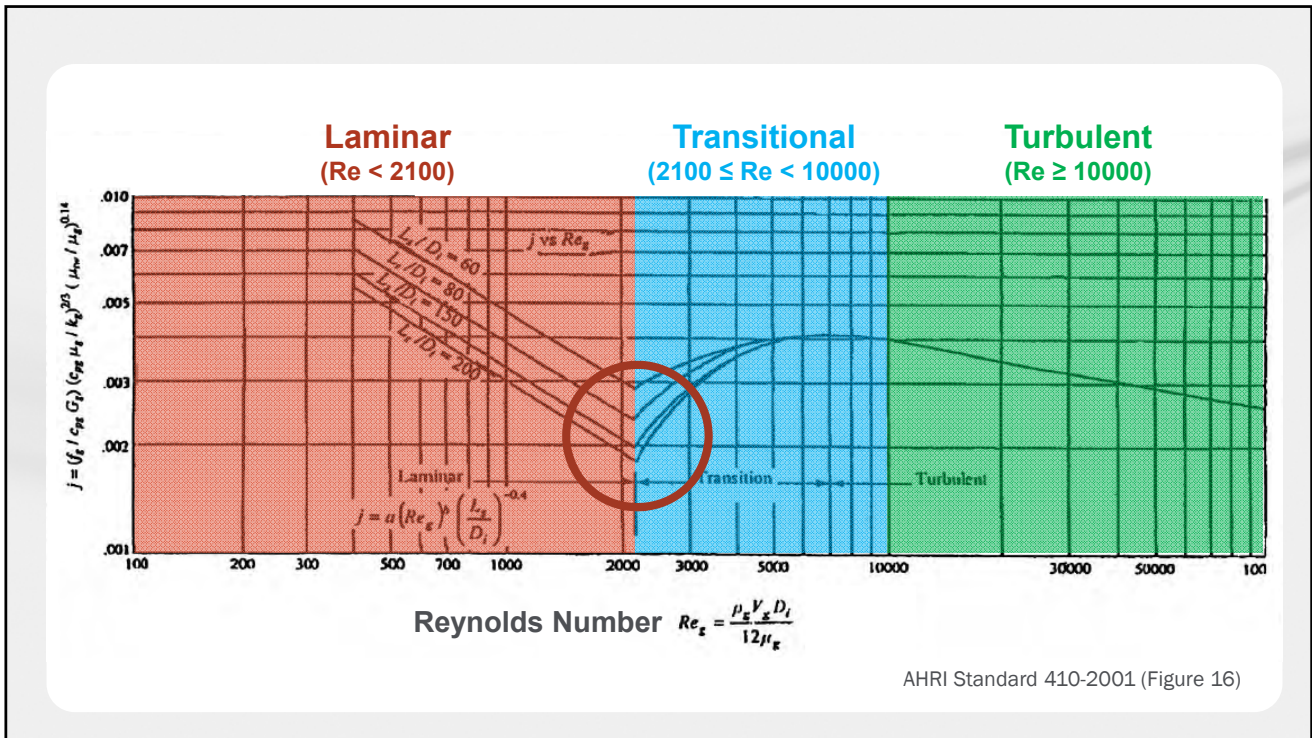


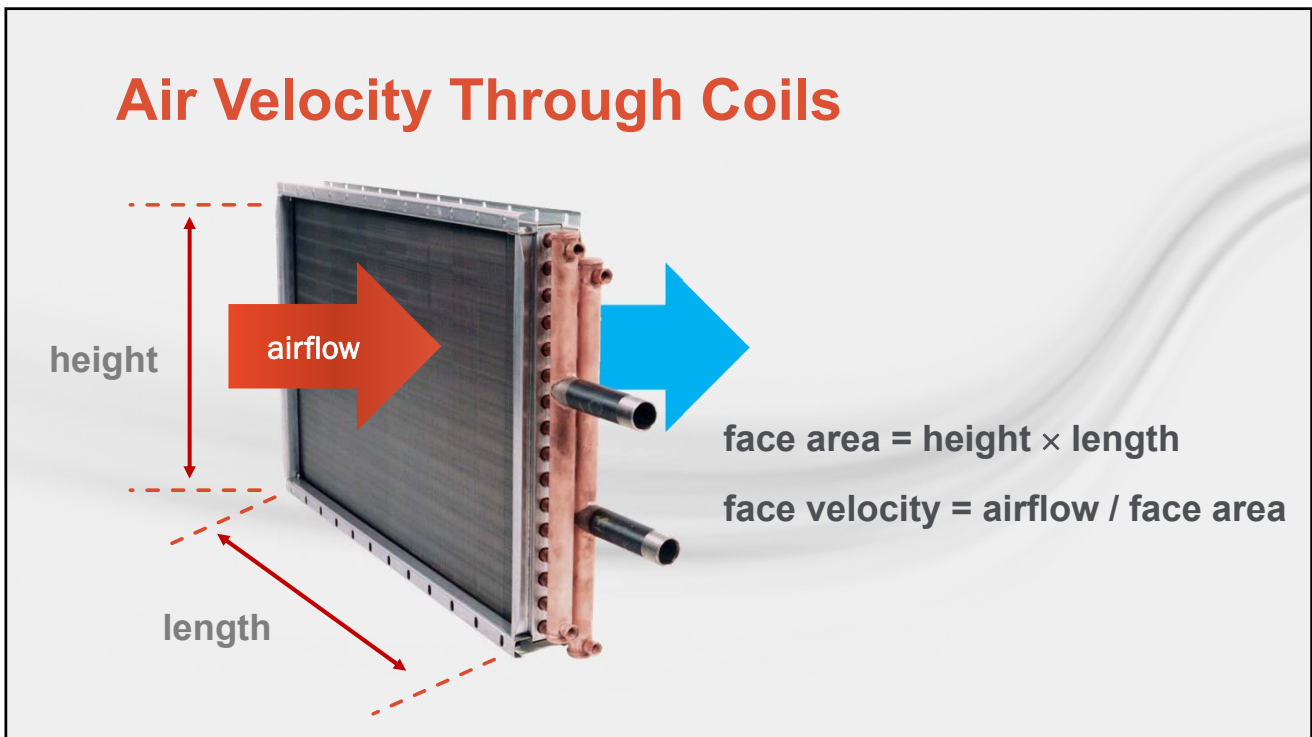
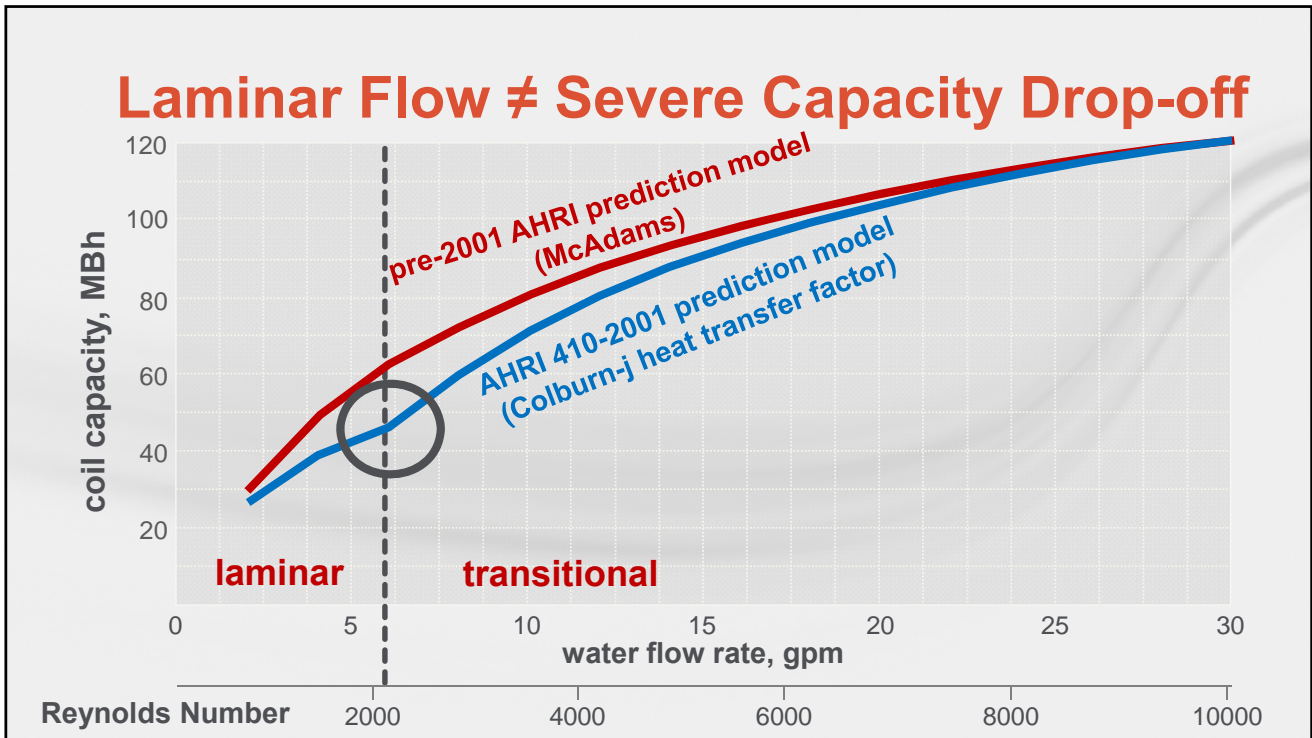
Guidelines for Water Velocity



Guidelines for Water Velocity







Air Velocity-Related Concerns

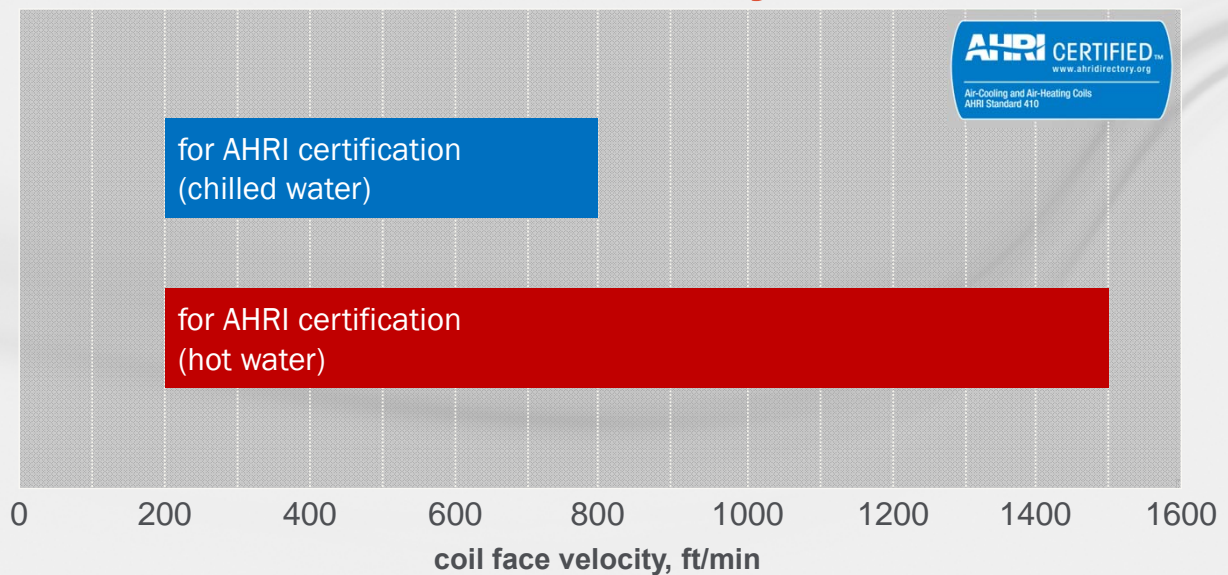
Air velocity too low:

- Non-uniform leaving-air temperatures
- Less accurate prediction of coil capacity

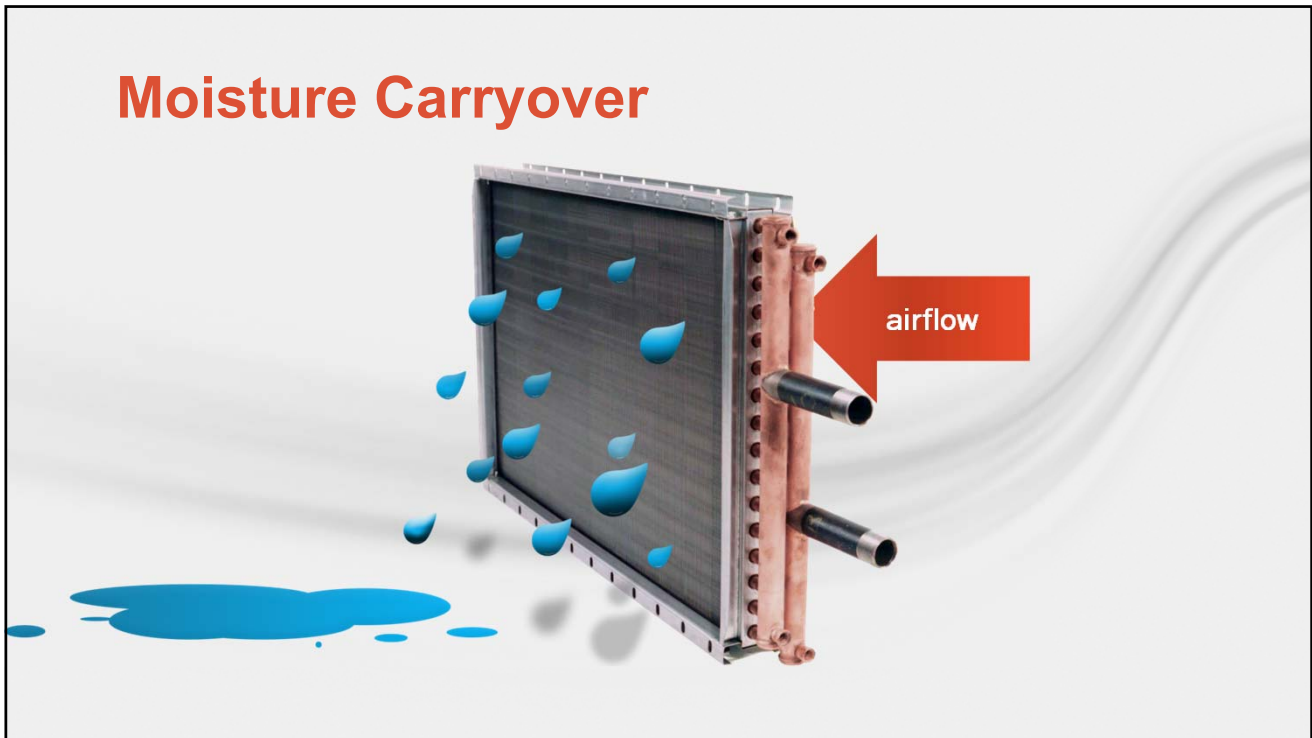
Air velocity too high:

- Noise
- High air pressure drop
- Risk of moisture carryover

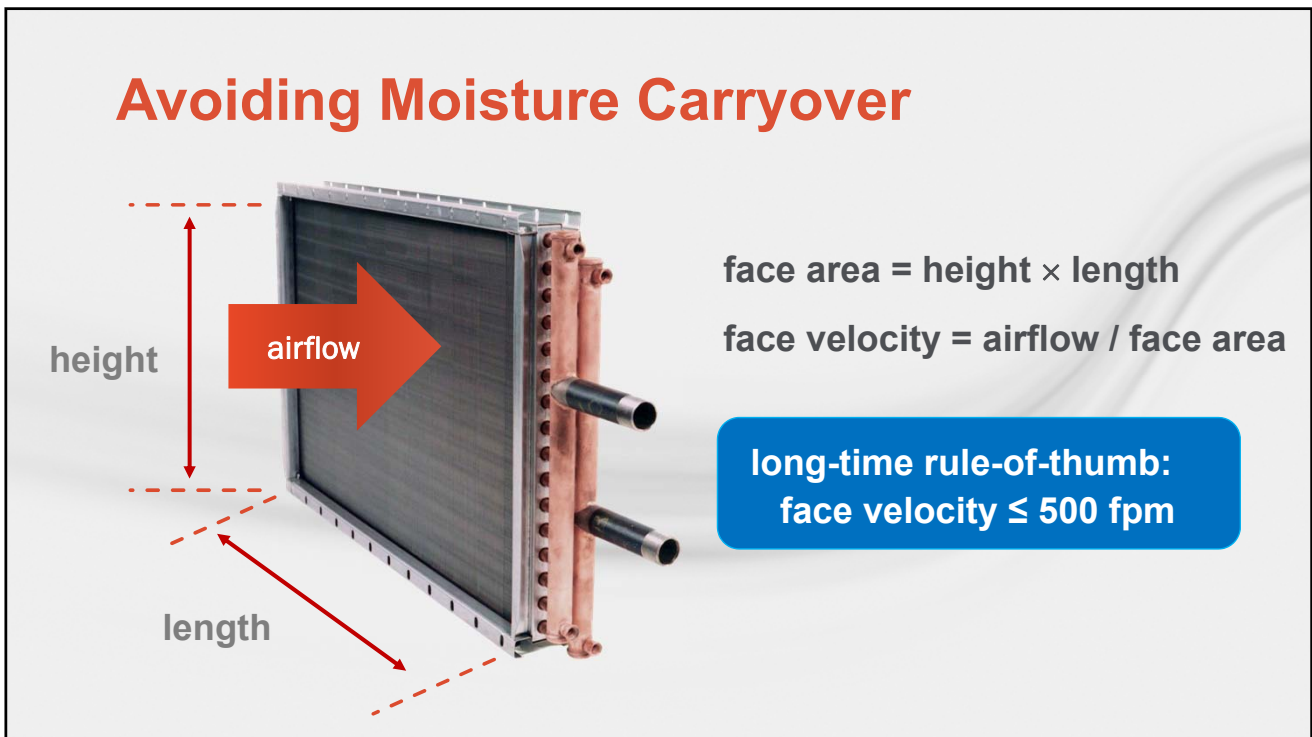
Guidelines for Air Velocity



Moisture Carryover

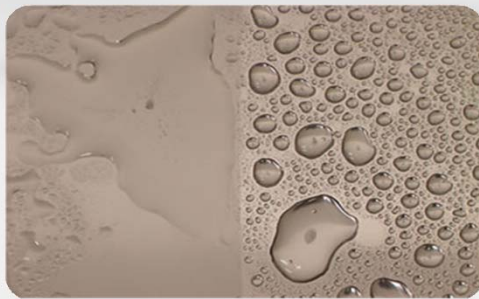


Avoiding Moisture Carryover

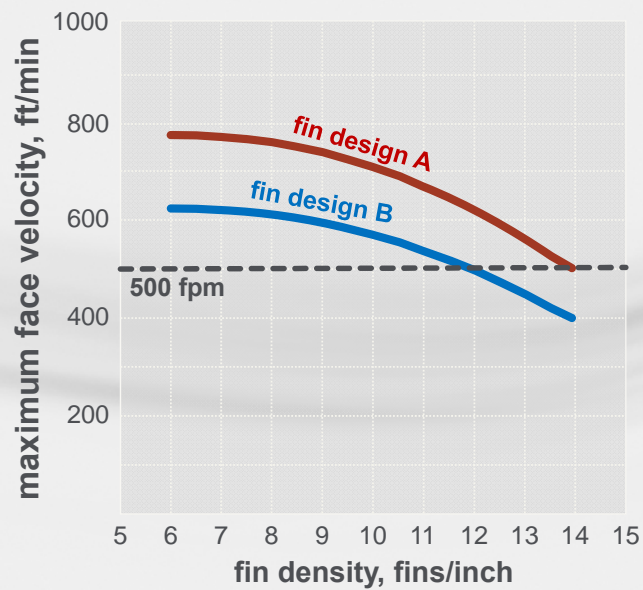


Factors Influencing Moisture Carryover

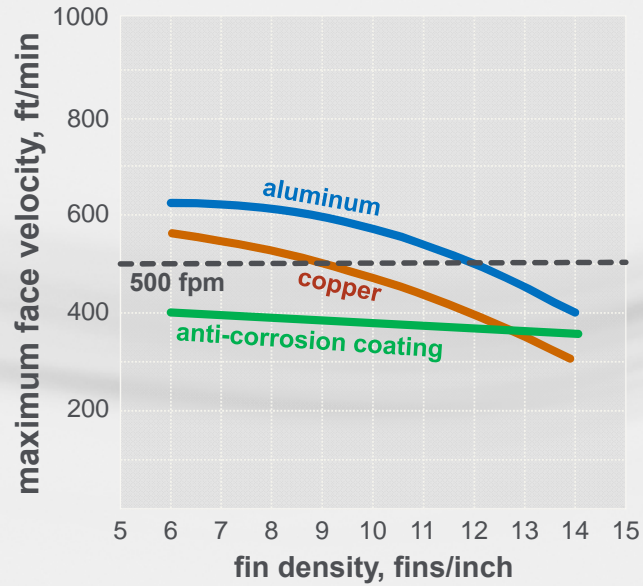
- Air velocity
- Fin design and material
- Number of fins
- Fin surface wettability



Same Fin Material, Different Fin Designs



Different Fin Materials, Same Fin Design

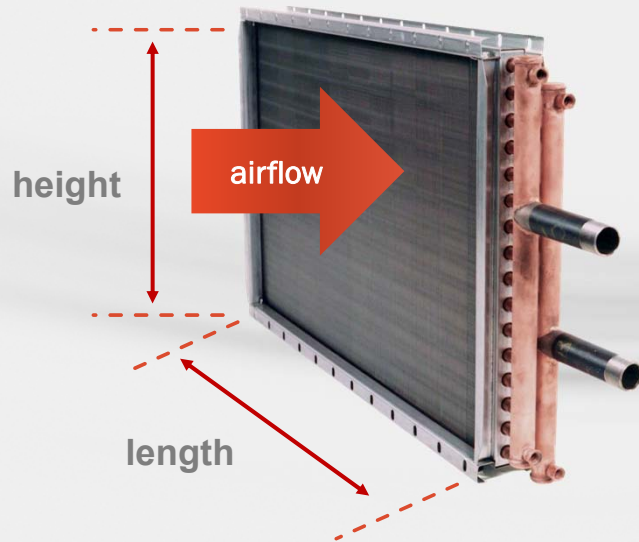


Agenda

- Water and air velocity ranges
- Coil selection examples
 - **Chilled-water coils**
 - Hot-water coils
- Freeze protection

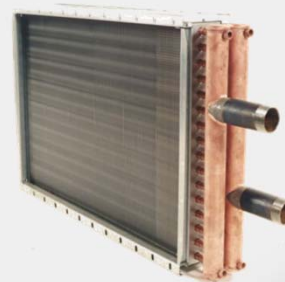
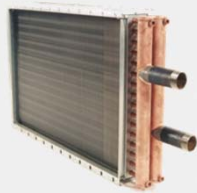


Coil Face Area and Face Velocity



face area = height × length

face velocity = airflow / face area

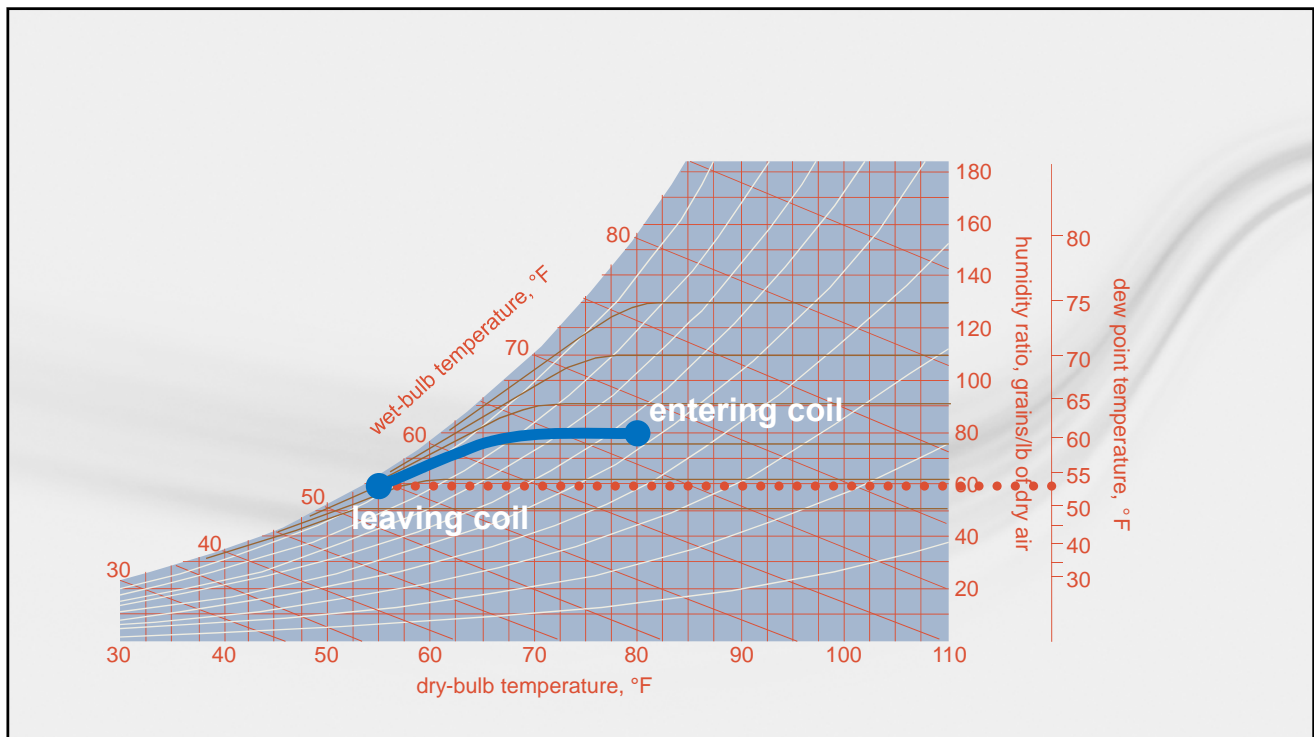
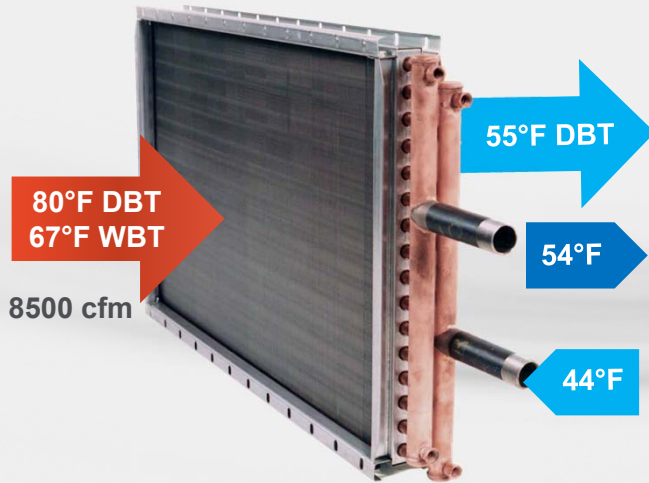


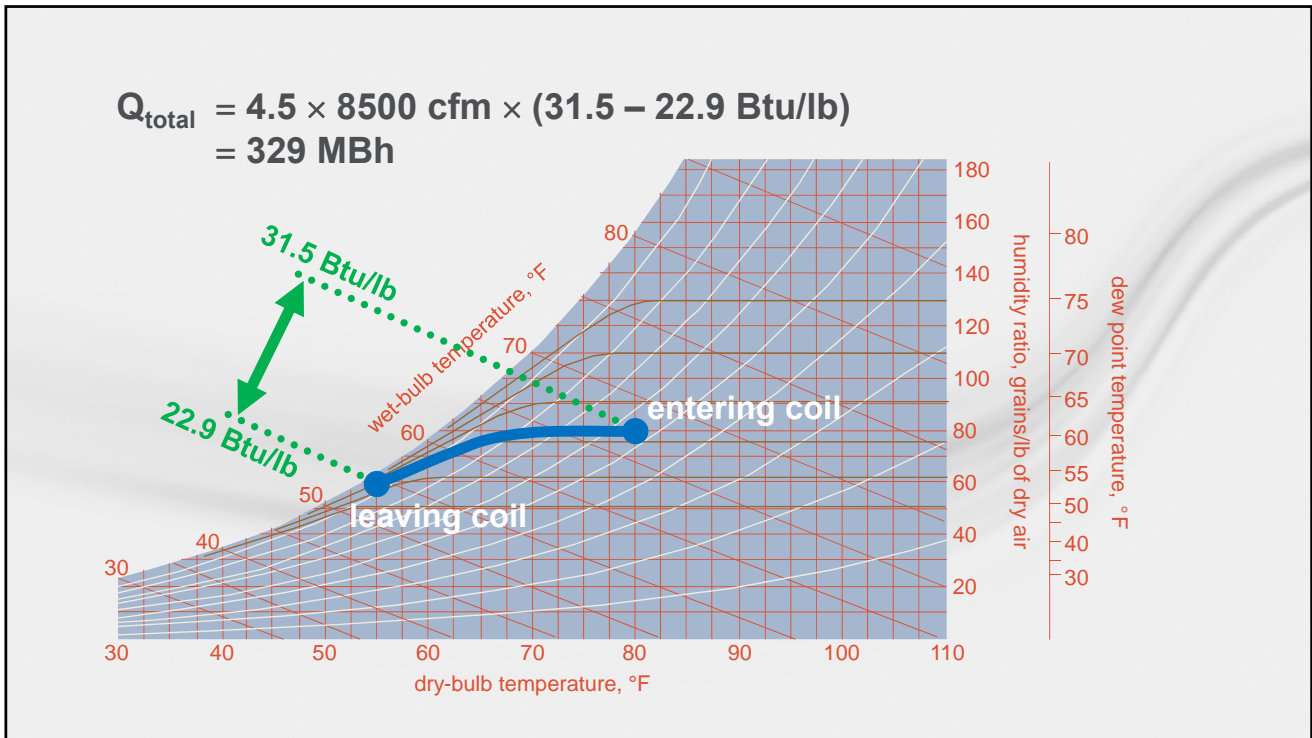
initial cost of coil
 size of AHU cabinet
 initial cost of AHU
 air pressure drop
 fan energy use
 water pressure drop
 pump energy use

LOWER
 SMALLER
 LOWER
 HIGHER
 HIGHER
 HIGHER
 HIGHER

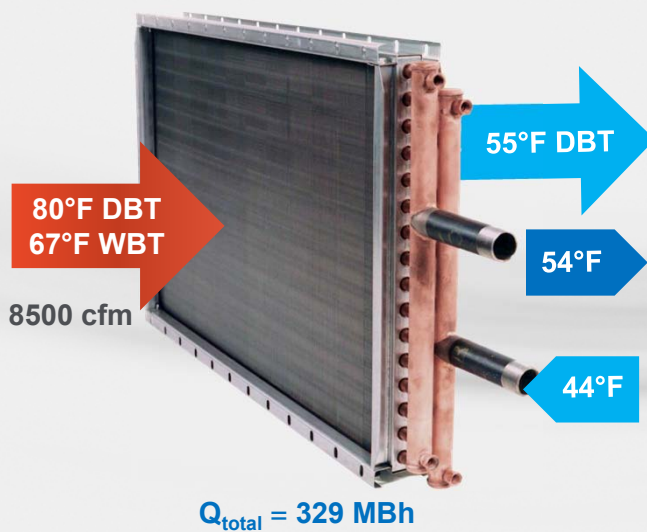
HIGHER
 LARGER
 HIGHER
 LOWER
 LOWER
 LOWER
 LOWER

Example #1: Coil Face Area

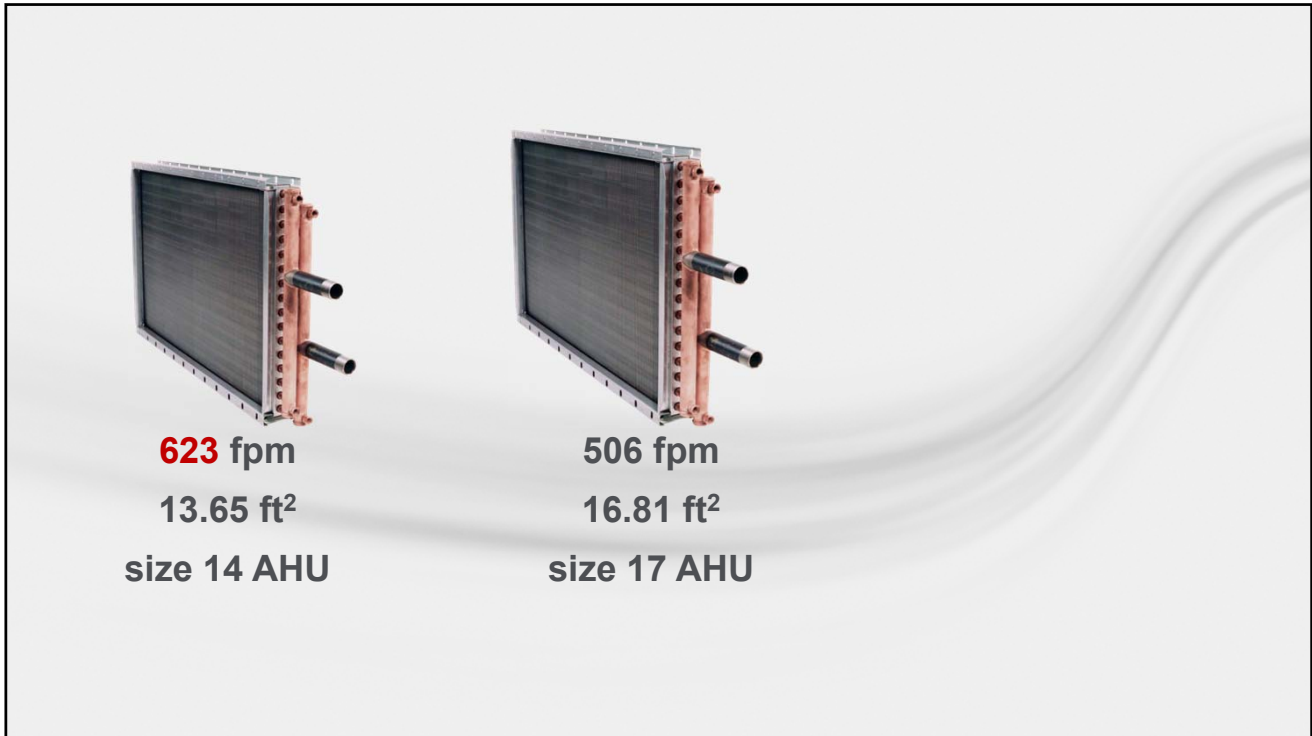




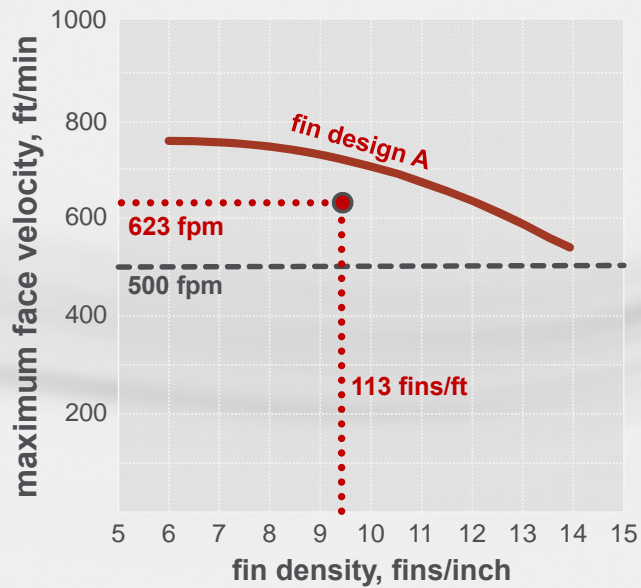
Traditional Selection at 500 fpm

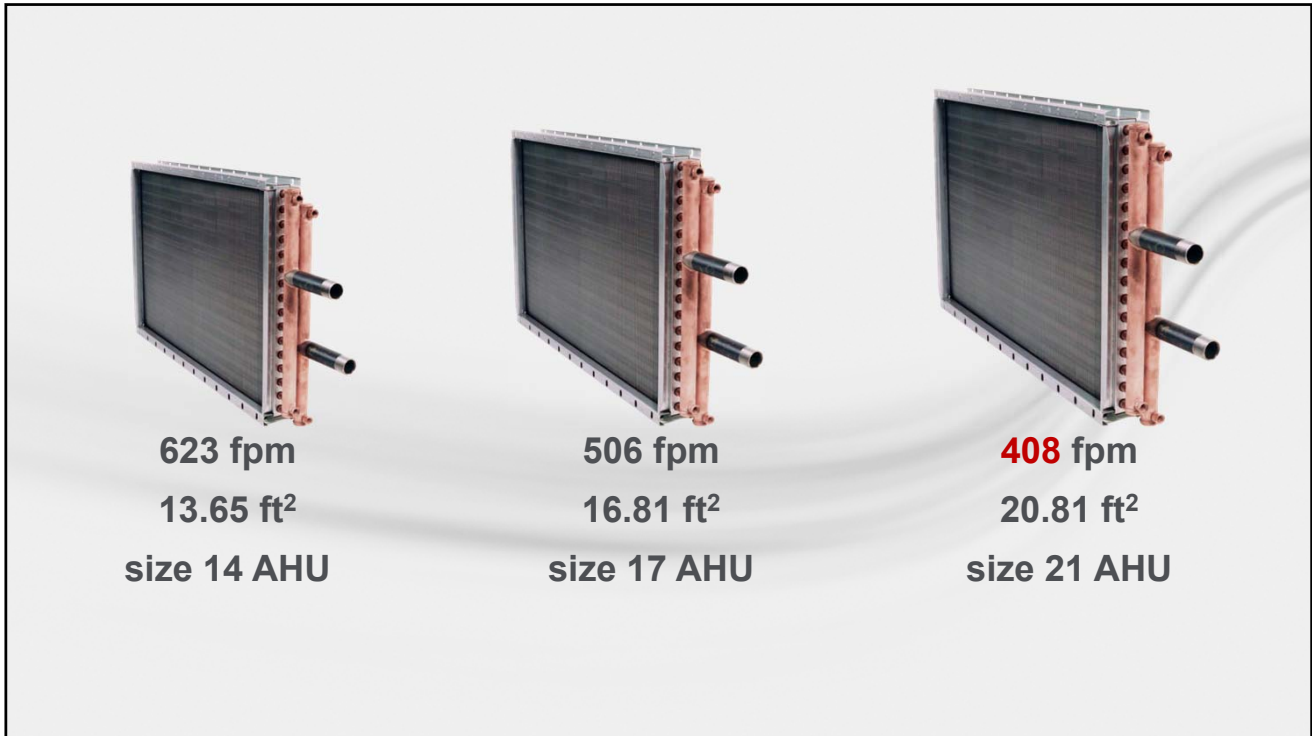


face area = airflow / face velocity
 $= 8500 \text{ cfm} / 500 \text{ fpm}$
 $= 17 \text{ ft}^2$



Moisture Carryover?



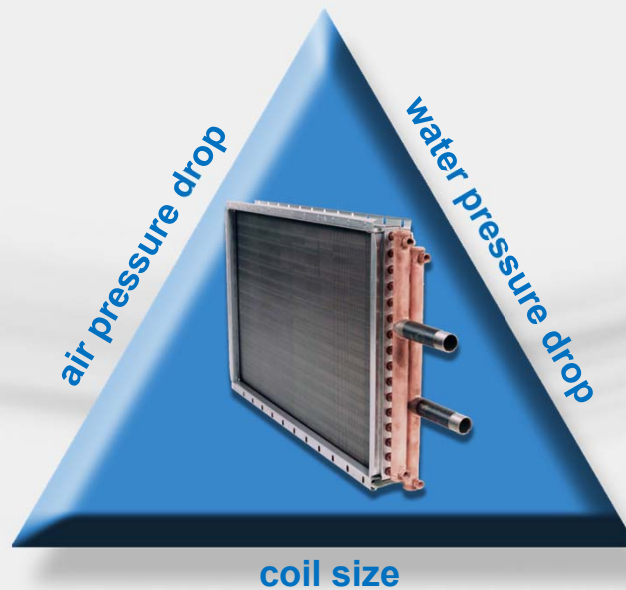


| | | | |
|--|------|------|------|
| coil face area, ft ² | 14 | 17 | 21 |
| face velocity, ft/min | 623 | 506 | 408 |
| coil rows | 6 | 6 | 4 |
| coil fins, fins/ft | 113 | 95 | 147 |
| water flow rate, gpm | 65.6 | 65.6 | 65.6 |
| water velocity, ft/sec | 4.5 | 3.6 | 3.3 |
| water pressure drop, ft H ₂ O | 11.5 | 8.2 | 5.9 |
| air pressure drop, in H ₂ O | 1.0 | 0.68 | 0.42 |



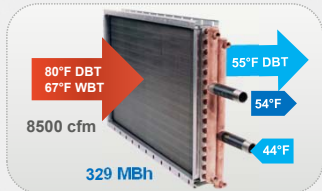
| | | | |
|--|------|------|------|
| coil face area, ft ² | 14 | 17 | 21 |
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| coil fins, fins/ft | 113 | 95 | 147 |
| water flow rate, gpm | 65.6 | 65.6 | 65.6 |
| water velocity, ft/sec | 4.5 | 3.6 | 3.3 |
| water pressure drop, ft H ₂ O | 11.5 | 8.2 | 5.9 |
| air pressure drop, in H ₂ O | 1.0 | 0.68 | 0.42 |

Example #2: APD versus WPD



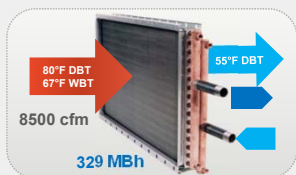
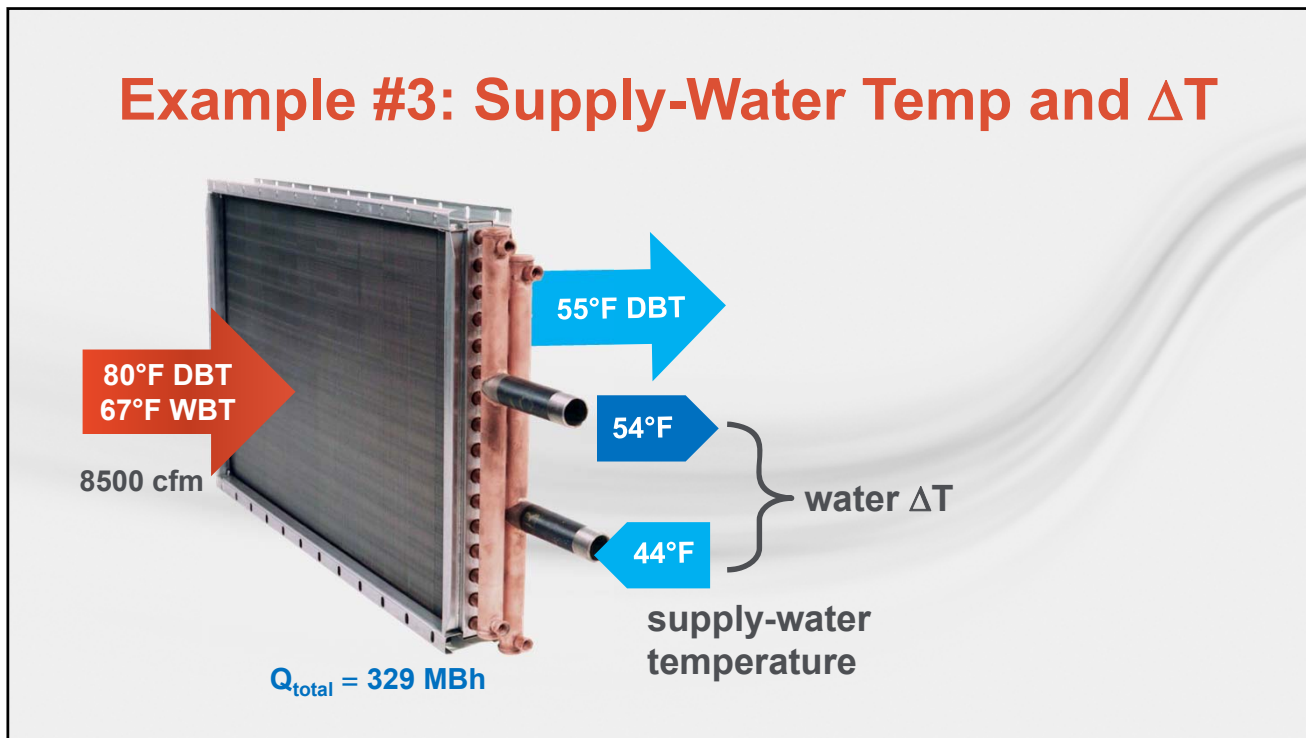


| | | | |
|--|-----------------|---------------|------------------------------------|
| coil face area, ft ² | 14 | 14 | 14 |
| coil rows | 6 | 8 | 6 |
| coil fins, fins/ft | 113 | 102 | 95 |
| coil circuiting | single-row feed | dual-row feed | single-row feed (with turbulators) |
| water flow rate, gpm | 65.6 | 65.6 | 65.6 |
| water velocity, ft/sec | 4.5 | 2.3 | 4.5 |
| water pressure drop, ft H ₂ O | 11.5 | 2.8 | 26.0 |
| air pressure drop, in H ₂ O | 1.00 | 1.25 | 0.93 |
| cost of the coil | base | base + 31% | base + 12% |

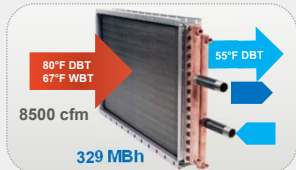


| | | | |
|--|-----------------|---------------|------------------------------------|
| coil face area, ft ² | 14 | 14 | 14 |
| coil rows | 6 | 8 | 6 |
| coil fins, fins/ft | 113 | 102 | 95 |
| coil circuiting | single-row feed | dual-row feed | single-row feed (with turbulators) |
| water flow rate, gpm | 65.6 | 65.6 | 65.6 |
| water velocity, ft/sec | 4.5 | 2.3 | 4.5 |
| water pressure drop, ft H ₂ O | 11.5 | 2.8 | 26.0 |
| air pressure drop, in H ₂ O | 1.00 | 1.25 | 0.93 |
| cost of the coil | base | base + 31% | base + 12% |

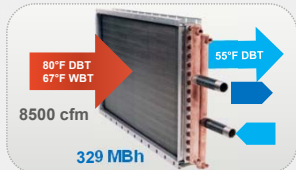
Example #3: Supply-Water Temp and ΔT



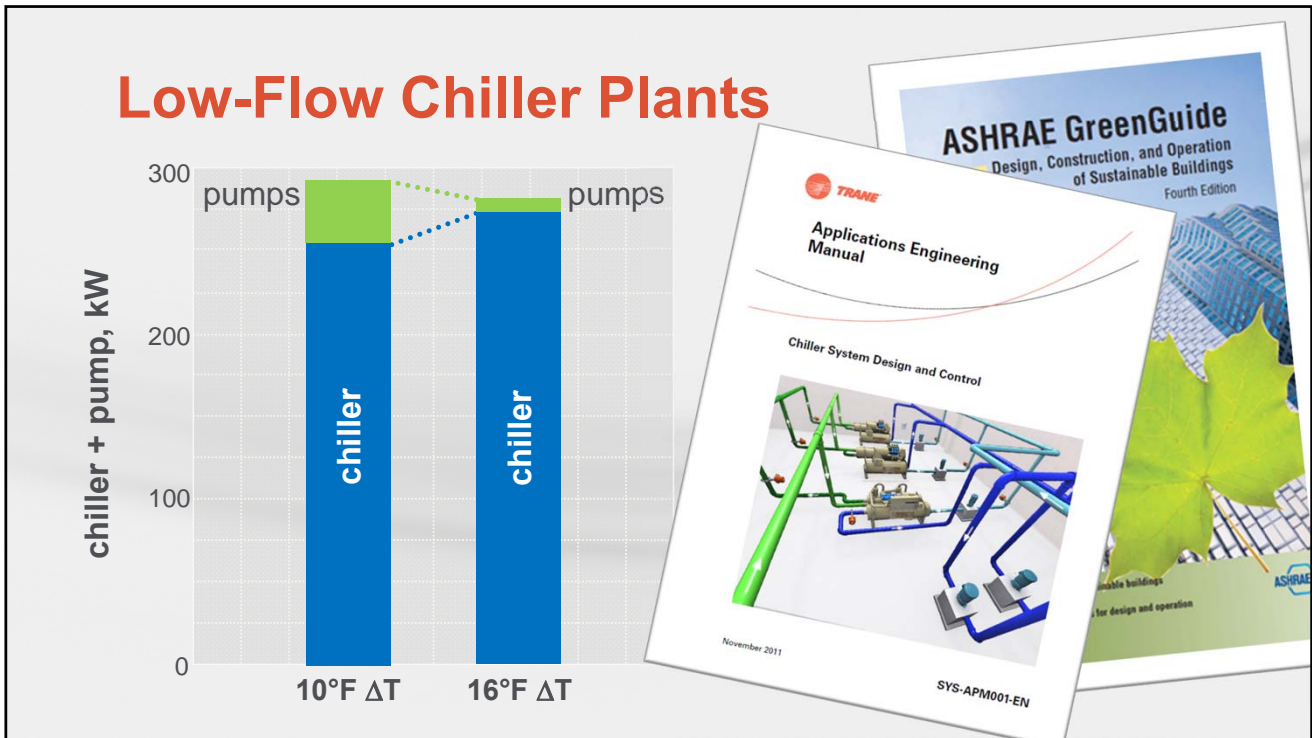
| | | |
|--|------|-----------|
| coil face area, ft ² | 17 | 17 |
| coil rows | 6 | 6 |
| coil fins, fins/ft | 95 | 127 |
| supply water temperature, °F | 44 | 44 |
| return water temperature, °F | 54 | 57 |
| water ΔT , °F | 10 | 13 |
| water flow rate, gpm | 65.6 | 50.4 |
| water velocity, ft/sec | 3.6 | 2.8 |
| water pressure drop, ft H ₂ O | 8.2 | 5.1 |
| air pressure drop, in H ₂ O | 0.68 | 0.77 |
| cost of the coil | base | base + 7% |



| | | | |
|--|------|-----------|-----------|
| coil face area, ft ² | 17 | 17 | 17 |
| coil rows | 6 | 6 | 6 |
| coil fins, fins/ft | 95 | 127 | 99 |
| supply water temperature, °F | 44 | 44 | 42 |
| return water temperature, °F | 54 | 57 | 55 |
| water ΔT, °F | 10 | 13 | 13 |
| water flow rate, gpm | 65.6 | 50.4 | 50.4 |
| water velocity, ft/sec | 3.6 | 2.8 | 2.8 |
| water pressure drop, ft H ₂ O | 8.2 | 5.1 | 5.1 |
| air pressure drop, in H ₂ O | 0.68 | 0.77 | 0.68 |
| cost of the coil | base | base + 7% | base + 1% |



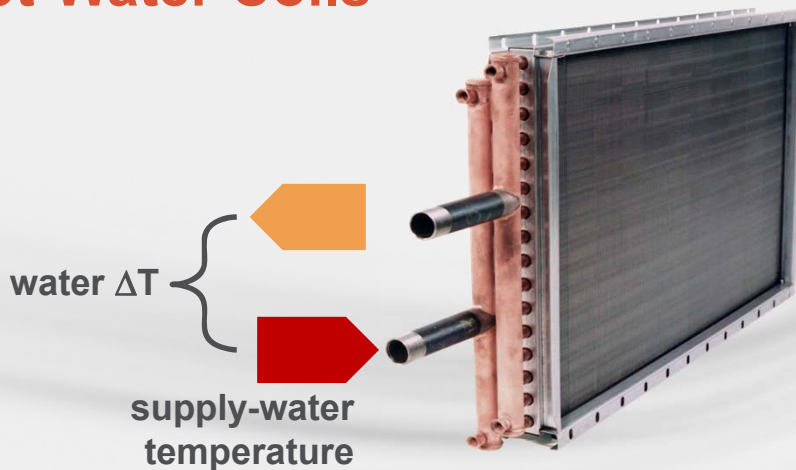
| | | | | |
|--|------|-----------|-----------|------------|
| coil face area, ft ² | 17 | 17 | 17 | 17 |
| coil rows | 6 | 6 | 6 | 4 |
| coil fins, fins/ft | 95 | 127 | 99 | 141 |
| supply water temperature, °F | 44 | 44 | 42 | 40 |
| return water temperature, °F | 54 | 57 | 55 | 56 |
| water ΔT, °F | 10 | 13 | 13 | 16 |
| water flow rate, gpm | 65.6 | 50.4 | 50.4 | 41.0 |
| water velocity, ft/sec | 3.6 | 2.8 | 2.8 | 2.3 |
| water pressure drop, ft H ₂ O | 8.2 | 5.1 | 5.1 | 5.8 |
| air pressure drop, in H ₂ O | 0.68 | 0.77 | 0.68 | 0.56 |
| cost of the coil | base | base + 7% | base + 1% | base – 16% |



Agenda

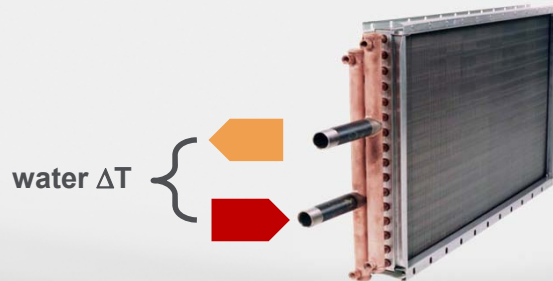
- Water and air velocity ranges
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 - **Hot-water coils**
- Freeze protection

Hot-Water Coils

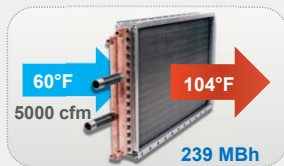


| | | | |
|--|------|-----------|-----------|
| coil face area, ft ² | 10 | 10 | 10 |
| coil rows | 2 | 2 | 2 |
| coil fins, fins/ft | 79 | 95 | 118 |
| supply water temperature, °F | 180 | 180 | 180 |
| return water temperature, °F | 160 | 150 | 140 |
| water ΔT, °F | 20 | 30 | 40 |
| water flow rate, gpm | 23.8 | 15.9 | 11.9 |
| water velocity, ft/sec | 1.9 | 1.2 | 0.9 |
| water pressure drop, ft H ₂ O | 0.94 | 0.44 | 0.25 |
| air pressure drop, in H ₂ O | 0.14 | 0.15 | 0.16 |
| cost of the coil | base | base + 2% | base + 6% |

Selecting HW Coils with a Larger ΔT



| water ΔT | SMALLER | LARGER |
|----------------------|---------|--------|
| initial cost of coil | LESS | MORE |
| air pressure drop | LESS | HIGHER |
| water flow rate | HIGHER | LOWER |
| water pressure drop | HIGHER | LOWER |



| | | | |
|--|------|------------|------------|
| coil face area, ft ² | 10 | 10 | 10 |
| coil rows | 2 | 4 | 4 |
| coil fins, fins/ft | 79 | 72 | 89 |
| supply water temperature, °F | 180 | 150 | 150 |
| return water temperature, °F | 160 | 120 | 110 |
| water ΔT , °F | 20 | 30 | 40 |
| water flow rate, gpm | 23.8 | 16.0 | 12.0 |
| water velocity, ft/sec | 1.9 | 1.2 | 0.9 |
| water pressure drop, ft H ₂ O | 0.94 | 0.64 | 0.38 |
| air pressure drop, in H ₂ O | 0.14 | 0.28 | 0.29 |
| cost of the coil | base | base + 75% | base + 80% |

Types of Boilers

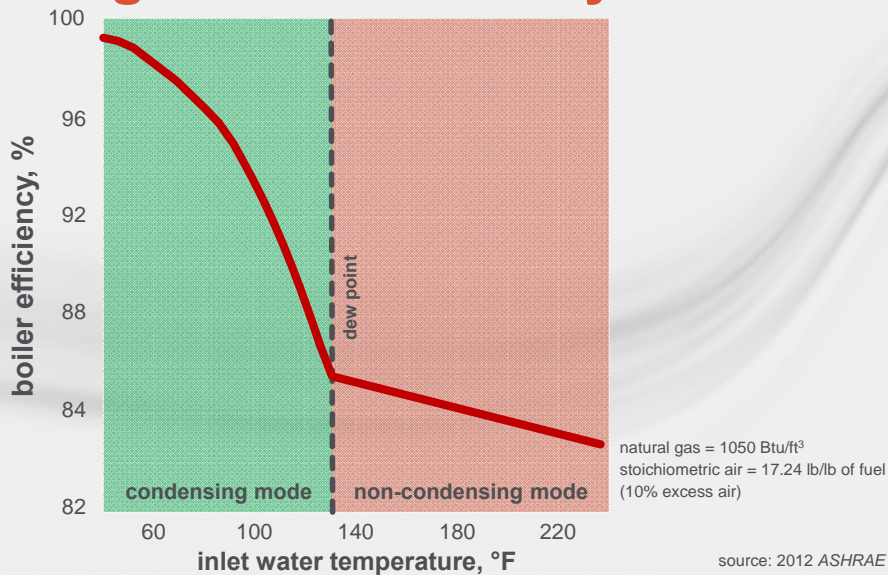
non-condensing boilers

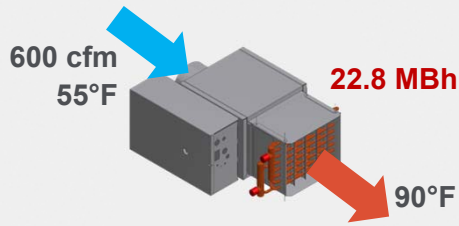
- Avoids condensing of flue gas (uses only sensible heat value of the fuel)
- Designed and operated to ensure water returns $\geq 140^{\circ}\text{F}$

condensing boilers

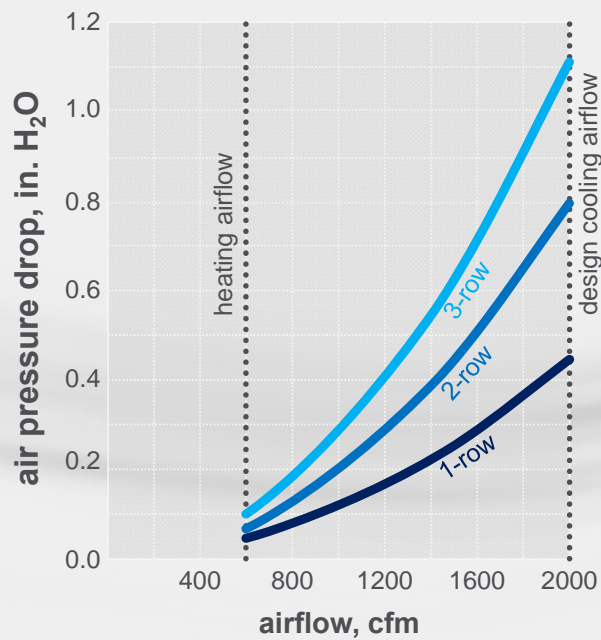
- Allows condensing of flue gas (uses some of the latent heat value of the fuel)
- More efficient with a lower return-water temperature

Condensing Boiler Efficiency

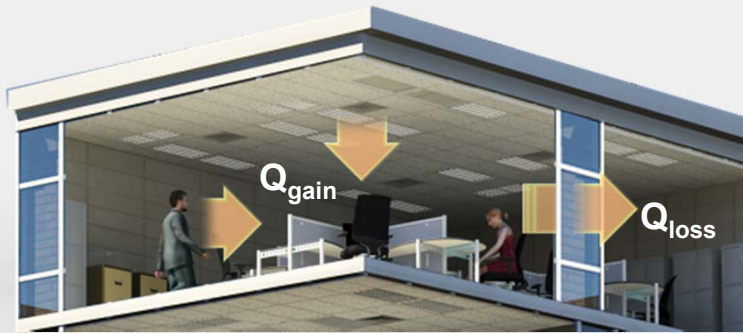




| | | | |
|---|------|------------|------------|
| coil rows | 1 | 2 | 3 |
| supply water temperature, °F | 180 | 150 | 150 |
| return water temperature, °F | 137 | 116 | 106 |
| water flow rate, gpm | 1.05 | 1.32 | 1.04 |
| water pressure drop, ft H ₂ O | 0.69 | 0.11 | 0.10 |
| air pressure drop, in H ₂ O (at design cooling airflow, 2000 cfm) | 0.45 | 0.79 | 1.10 |
| air pressure drop, in H ₂ O (at heating airflow, 600 cfm) | 0.04 | 0.07 | 0.10 |



Heating Mode vs. Reheat Mode



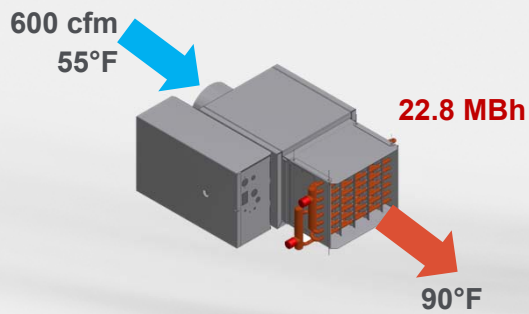
“heating” mode

$$Q_{loss} > Q_{gain}$$

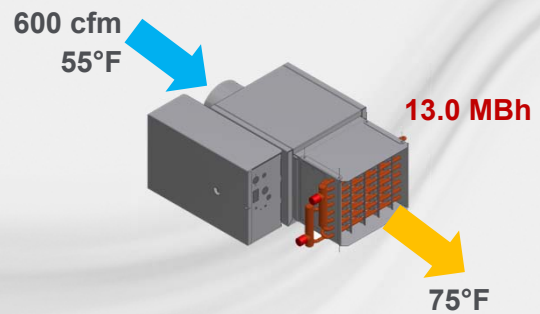
“reheat” mode

$$Q_{loss} \leq Q_{gain}$$

Heating Mode vs. Reheat Mode



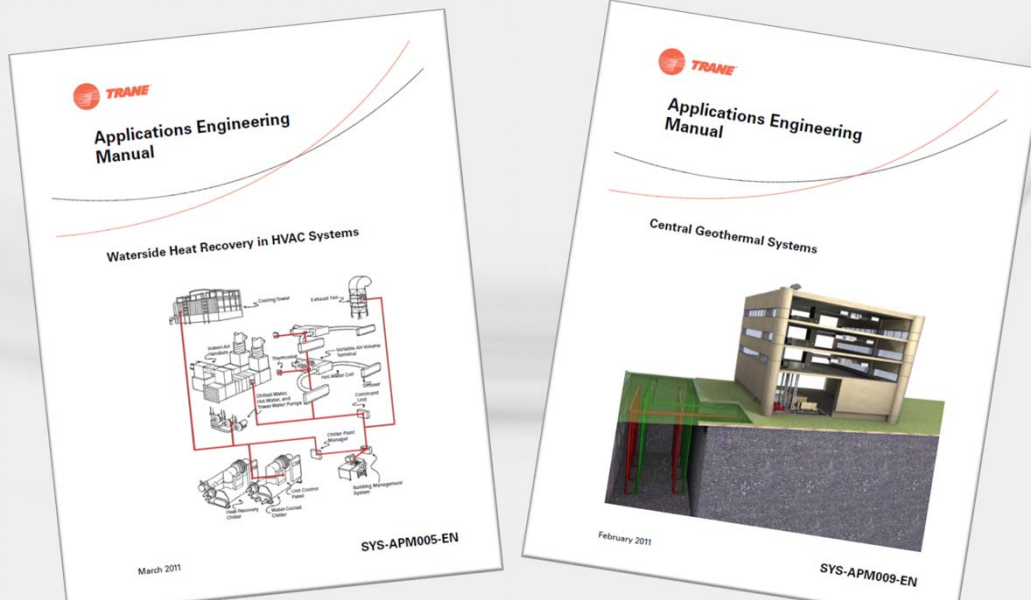
“heating” mode



“reheat” mode

| | | | | |
|--|---|------|------------|------------|
| heating | coil rows | 1 | 2 | 3 |
| | air pressure drop, in H ₂ O (at design cooling airflow, 2000 cfm) | 0.45 | 0.79 | 1.10 |
| | air pressure drop, in H ₂ O (at minimum airflow, 600 cfm) | 0.04 | 0.07 | 0.10 |
| | heating capacity, MBh | 22.8 | 22.8 | 22.8 |
| | supply water temperature, °F | 180 | 150 | 150 |
| | return water temperature, °F | 137 | 116 | 106 |
| | water flow rate, gpm | 1.05 | 1.32 | 1.04 |
| water pressure drop, ft H ₂ O | 0.69 | 0.12 | 0.10 | |
| reheat | heating capacity, MBh | 13.0 | 13.0 | 13.0 |
| | supply water temperature, °F | 150 | 105 | 105 |
| | return water temperature, °F | 103 | 91 | 86 |
| | water flow rate, gpm | 0.56 | 1.86 | 1.41 |
| | water pressure drop, ft H ₂ O | 0.23 | 0.21 | 0.17 |

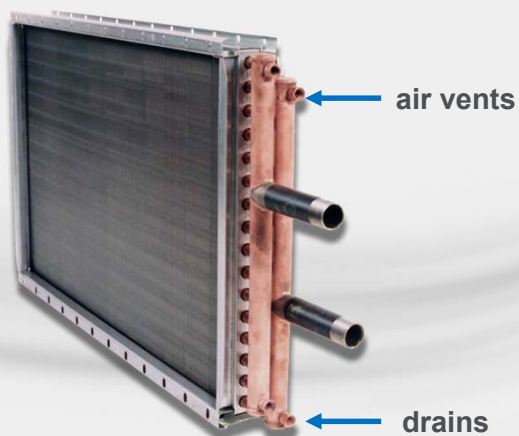
Chiller Plants with Heat Recovery



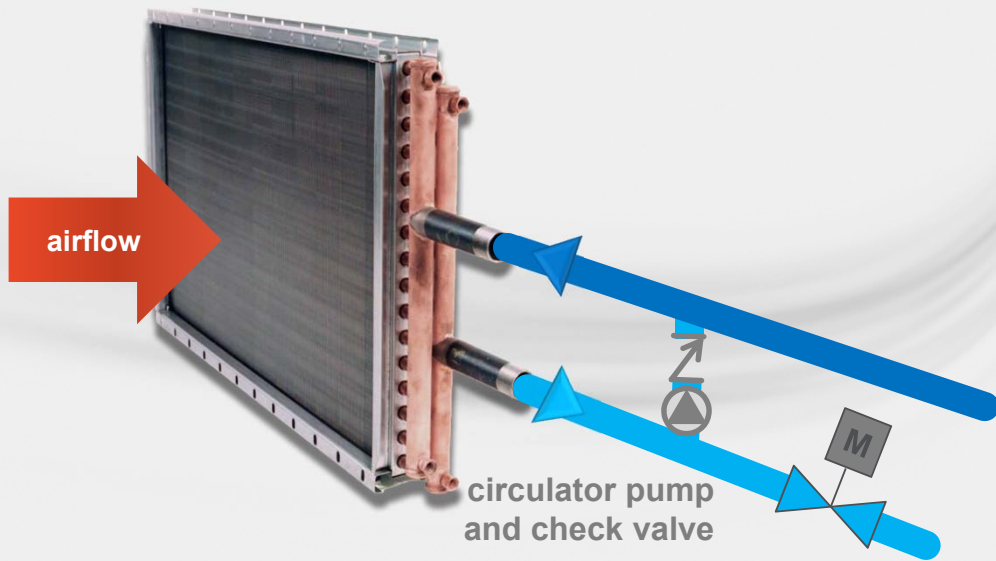
Agenda

- Water and air velocity ranges
- Coil selection examples
 - Chilled-water coils
 - Hot-water coils
- **Freeze protection**

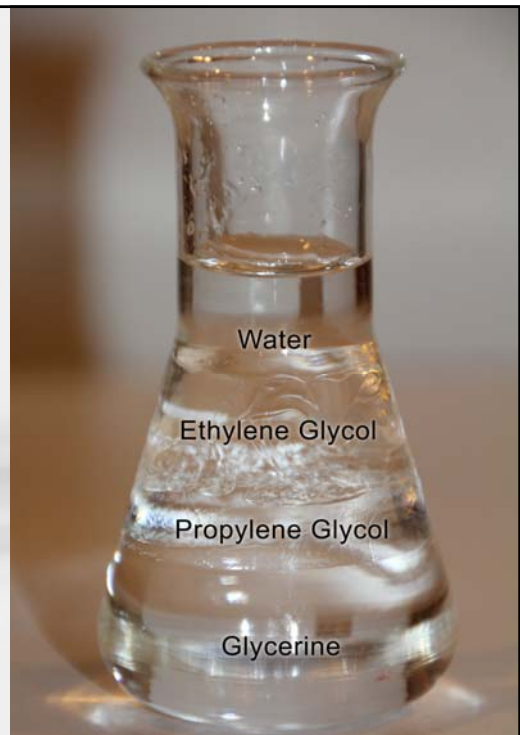
Drain Cooling Coils During Cold Weather



Coil Pumping



Add Antifreeze (e.g., Glycol)



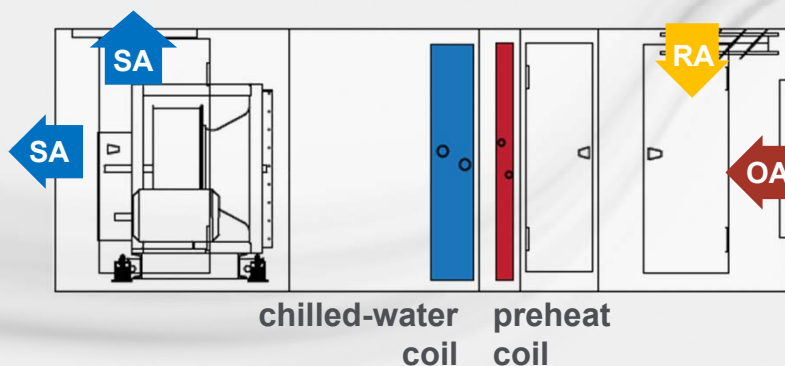
Freeze Protection vs. Burst Protection

| fluid temperature | ethylene glycol concentration (% volume) | | propylene glycol concentration (% volume) | |
|-------------------|--|------------------|---|------------------|
| | freeze protection | burst protection | freeze protection | burst protection |
| 20°F | 16% | 11% | 18% | 12% |
| 10°F | 25% | 17% | 29% | 20% |
| 0°F | 33% | 22% | 36% | 24% |
| -10°F | 39% | 26% | 42% | 28% |
| -20°F | 44% | 30% | 46% | 30% |
| -30°F | 48% | 30% | 50% | 33% |
| -40°F | 52% | 30% | 54% | 35% |
| -50°F | 56% | 30% | 57% | 35% |
| -60°F | 60% | 30% | 60% | 35% |

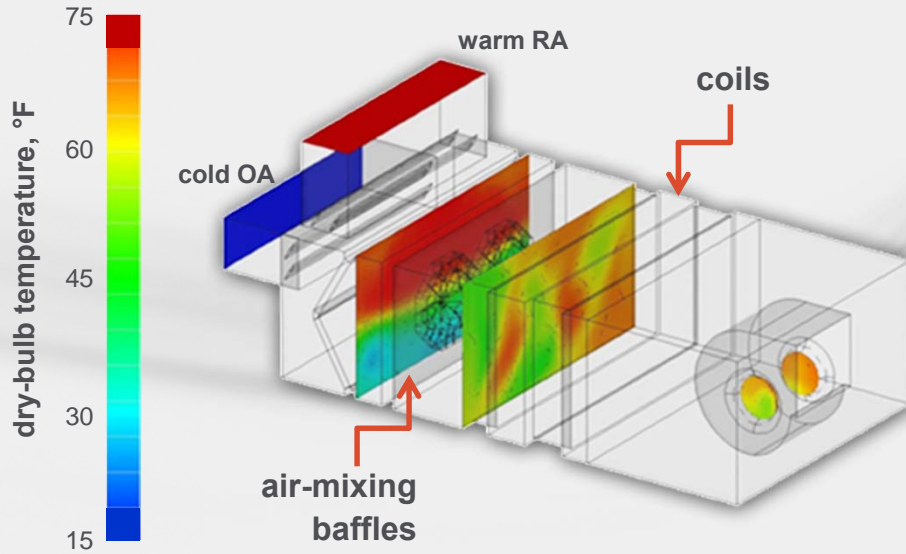
source: Dow Chemical Company. 2008. *Heat Transfer Fluids for HVAC and Refrigeration Systems.*

Preheat the Entering Air

- Electric heater
- Hot-water or steam coil
- Air-to-air energy recovery device (e.g., wheel)



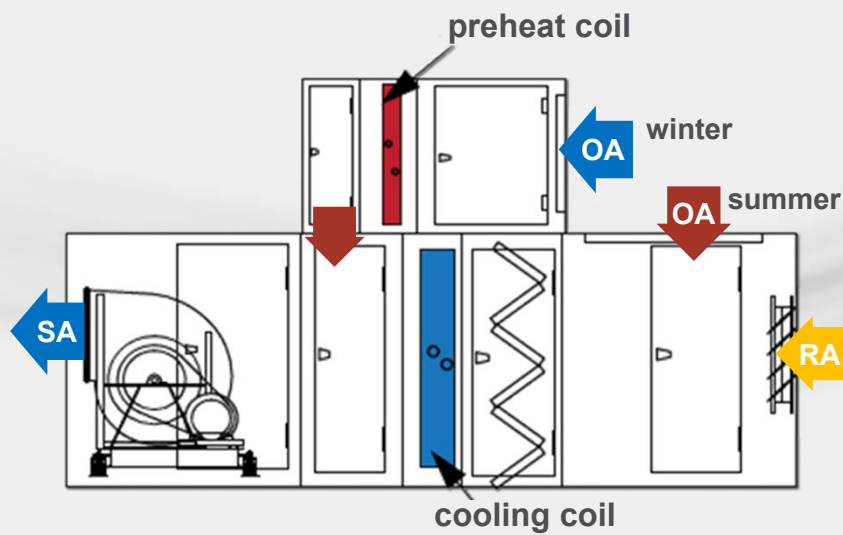
Use Air-Mixing Baffles



source: Blender Products, Inc.

introduce outdoor air downstream of the cooling coil

Dual-Path Air Handler

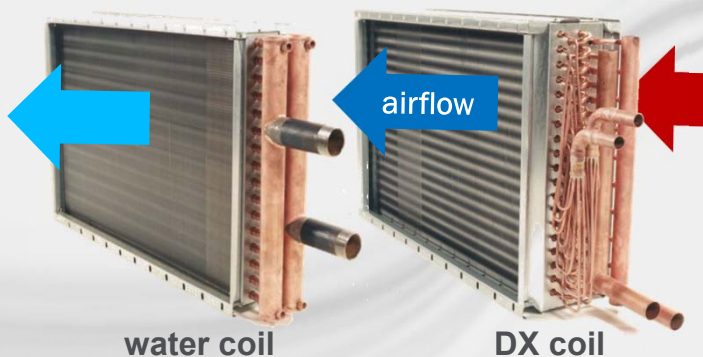


Coil Freeze Protection Options

- Drain chilled-water coils during cold weather
- Coil pumping
- Add antifreeze to the chilled- or hot-water system
- Preheat the entering air
- Use air-mixing baffles
- Introduce outdoor air downstream of the cooling coil

Water Coil Downstream of a DX Coil

- Low airflow through the DX coil?
- Compressor operating when the fan is off?
- Split system resulting in too low a SST?
- Too low of temperature entering DX coil?



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- Demand-controlled ventilation
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- Ice Storage Design and Control
- All Variable-Speed Chiller Plant Operation



Remaining 2015 Programs

- Acoustics: Evaluating Sound Data
- Small Chilled-Water Systems

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1. Which industry standard establishes a common set of testing and rating requirements for determining the capacity and pressure drops of cooling and heating coils?
 - a. ASHRAE Standard 62.1
 - b. AHRI Standard 410
 - c. AHRI Standard 550/590
 - d. ASHRAE Standard 90.1
2. Which of the following are concerns regarding too high of water velocity through the tubes of a coil? Choose all that apply.
 - a. Risk of water droplets blowing off the outer surfaces of the fins (i.e., carryover).
 - b. Risk of erosion on the inside surfaces of the tubes.
 - c. Too much noise.
 - d. Air can become trapped inside the coil tubes, degrading heat transfer.
3. Which of the following are concerns regarding too high of air velocity through the face of the coil? Choose all that apply.
 - a. Risk of water droplets blowing off the outer surfaces of the fins (i.e., carryover).
 - b. Risk of erosion on the inside surfaces of the tubes.
 - c. Excessive air pressure drop.
 - d. Air can become trapped inside the coil tubes, degrading heat transfer.
4. True or False: Laminar water flow through the tubes of a coil results in a SEVERE drop-off in capacity.
5. Which of the following factors influence moisture carryover (water droplets blowing off the outer surfaces of the fins)? Choose all that apply.
 - a. Air velocity through the face of the coil.
 - b. How densely the fins are packed together.
 - c. Material the fins are made of.
 - d. Whether or not the surface of the fins have a coating applied to them.
6. True or False: As long as dehumidifying coils are selected for a face velocity less than 500 ft/min, no moisture carryover will occur, regardless of the fin material or fin density.
7. When selecting a cooling coil to provide the same required capacity, which of the following are benefits of selecting a coil with a larger face area (lower face velocity)? Choose all that apply.
 - a. Less fan energy use.
 - b. A smaller air handler cabinet is required to house the coil.
 - c. A warmer entering-air temperature.
 - d. Lower air pressure drop.
8. True or False: When selecting a cooling coil to provide the same required capacity, selecting the coil with a lower water flow rate (larger ΔT) results in more pumping energy and requires upsizing piping, valves, and pumps.
9. True or False: Newer, condensing-style boilers are more efficient when the temperature of the water entering the boiler is lower.
10. True or False: When specifying the amount of glycol to use in a chilled-water system, the concentration required to provide “burst” protection (to protect equipment from damage) is lower than the concentration required to provide “freeze” protection (to prevent any ice crystals from forming).